

**FINAL DRAINAGE AND EROSION
CONTROL REPORT**

FOR

**FIRST REPLAT OF PROSPECT
RIVERSIDE SUBDIVISION
(RIVERSIDE STORAGE)**

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CONTROL REPORT**

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RIVERSIDE SUBDIVISION
(RIVERSIDE STORAGE)**

Prepared for:

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Prepared by:

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October 10, 2014

Job Number 264-02



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October 10, 2014

Glen Schlueter
City of Fort Collins Stormwater
700 Wood Street
Fort Collins, CO 80522-0580

RE: Final Drainage and Erosion Control Report for First Replat of Prospect Riverside Subdivision (Riverside Storage)

Dear Glen,

I am pleased to submit for your review and approval, this Final Drainage and Erosion Control Report for First Replat of Prospect Riverside Subdivision. I certify that this report for the drainage design was prepared in accordance with the criteria in the City of Fort Collins Storm Drainage Manual.

I appreciate your time and consideration in reviewing this submittal. Please call if you have any questions.

Sincerely,



Patricia Kroetch, P.E

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1. GENERAL LOCATION AND DESCRIPTION

1.1 Location

This site is located on the east side of Riverside Drive north of East Prospect Road in the Southeast Quarter of Section 18, Township 7 North, Range 68 West of the Sixth Principal Meridian, in the City of Fort Collins, Larimer County, Colorado. See the Vicinity Map in Appendix A of this report.

This project is bounded on the north by existing storage units, on the east by existing Union Pacific Railroad tracks, on the west by Riverside Drive, and on the south by existing Rivendell School.

1.2 Description of Property

The entire project consists of approximately 2.2 acres. The site is currently developed, with areas of existing asphalt and gravel. Existing slope is to the northeast with slopes ranging from approximately 1.5% to 3%. The site currently drains into an existing swale located at the northeast corner of the site.

Proposed development on-site will include one office building, five self-storage buildings, and associated drives, parking, and walks. Existing drainage patterns will not be significantly altered with this development.

2. DRAINAGE BASINS AND SUB-BASINS

2.1 Major Basin Description

The proposed development lies within the Spring Creek Drainage Basin. Both stormwater detention and extended water quality detention are required in this basin. The City requirement for stormwater detention in the Spring Creek basin is a single-stage detention with a 100-year release rate equal to the existing 2-year runoff.

2.2 Sub-basin Description

Runoff from this site currently flows to an existing swale located in the northeast corner of the site. From there, the runoff is conveyed in a proposed pipe and the existing swale to the north along the rear of the adjacent properties to an existing pipe under the railroad

tracks. The existing swale across the adjacent properties was determined to be a historic conveyance for this site. With the proposed drainage concept for this site, the detained runoff will continue to be released into the existing swale via a short outfall pipe.

3. DRAINAGE DESIGN CRITERIA

3.1 Regulations

This report was prepared to meet or exceed the “City of Fort Collins Storm Drainage Design Criteria Manual” specifications except where variances are requested as noted in Section 4.2 of this report. Where applicable, the criteria established in the “Urban Storm Drainage Criteria Manual” (UDFCD), 2001, developed by the Denver Regional Council of Governments, has been used.

3.2 Development Criteria Reference and Constraints

The runoff from this site has been routed to conform to the requirements of the City of Fort Collins Stormwater Department. Both stormwater runoff detention and extended water quality detention are required for this site and are being provided by the proposed on-site detention pond. The release rate from the site will be equal to the existing 2-year runoff.

3.3 Hydrologic Criteria

Runoff computations were prepared for the 2-year minor and 100-year major storm frequencies utilizing the rational method. All hydrologic calculations associated with the basins are included in Appendix B of this report. Standard Form 8 (SF-8) provides time of concentration calculations for all sub-basins.

Detention volume was calculated using the runoff rate for the 2-year rainfall event with existing site conditions, which includes existing sections of asphalt paving and gravel. The FAA method for detention pond sizing was utilized to determine the required volume. Water quality volume was calculated using the method recommended in the “Urban Storm Drainage Criteria Manual”. Refer to the detention calculations included in Appendix C of this report.

3.4 Hydraulic Criteria

Hydraulic elements have been designed per City of Fort Collins standards to adequately convey the 100-year storm runoff from this site to the proposed detention pond. An existing drainage swale will convey the detained runoff from the site to the downstream railroad crossing.

4. DRAINAGE FACILITY DESIGN

4.1 General Concept

The runoff from this site will flow into the parking lot and drive aisles which will be constructed using conventional materials (asphalt or concrete) and porous pavers. The runoff from the site will either flow on the surface or enter a perforated pipe via the porous pavers. In a situation where the porous pavements are clogged, the runoff will flow on the surface and enter the detention pond on the east side of the site. On-site runoff will also be conveyed to the detention pond via flows in LID swales along the north and south property boundaries. The detained runoff will discharge into the existing swale located at the northeast corner of the site. From there, runoff will be conveyed in the existing swale downstream to an existing railroad crossing. This existing swale may need to be cleaned out (with permission of the downstream property owner) to ensure adequate conveyance and removal of any obstructions.

4.2 Specific Flow Routing

With this design, the site is modeled as a single basin (Basin 1). This basin includes all of the proposed improvements on site including the office building, parking for the office building, the five storage buildings, the drives between the storage buildings, the sidewalks and all of the water quality enhancement features. The runoff from the site will follow the historic runoff path and will flow from the west (Riverside Avenue) to the east and into the detention area.

Drainage design for this site has been designed to convey on-site runoff to the proposed detention pond and incorporate the required water quality enhancement features. On-site runoff will be conveyed to the detention pond via surface flow in the drive aisles, in the LID swales and subsurface in the perforated pipes. The detention pond will release the detained runoff from the site at the existing (historic) 2-year runoff rate of 2 cfs. The

developed 2-year runoff rate for this Basin is 3.8 cfs and the developed 100-year runoff rate is 18.9 cfs.

One variance is requested for this project. A variance is being requested to reduce the minimum freeboard for the detention pond from 1.0' to 0.7'. This will not impact the structure on site or on the adjacent site.

4.3 Drainage Summary

This site has been designed to meet or exceed the “City of Fort Collins Storm Drainage Design Criteria Manual” specifications except where variances are requested as noted in Section 4.2 of this report. The proposed drainage design for this site has been designed to convey on-site runoff to the detention pond while minimizing future maintenance.

All drainage facilities proposed with this project, including the detention pond and outlet structure are private and will be owned and maintained by the property owner or Owner’s Association.

5. STORMWATER MANAGEMENT CONTROLS

5.1 Written Analysis

The soils on this site are classified by the USGS Soil Survey as Kim Loam with a small area of Santana Loam and are classified in the hydrologic group B. The soils are described as having a slow runoff rate and the hazard of water erosion is slight and the hazard of wind erosion is moderate.

The site is surrounded by developed sites including streets and paved areas. The construction shall utilize silt fence around the perimeter to control sediment transport from rainfall and from wind. The silt fence that is located in the proposed pavement areas will be removed prior to placing new pavement. Rock socks will be utilized in the existing curb and the newly constructed swales to capture sediments that are not fully contained by the silt fence placement. The locations of the rock socks will be in the areas of concentrated flow such as in the existing curb, at the new swales and on the existing concrete sidewalks as needed.

The site will also utilize a vehicle tracking control pad to minimize sediment from being tracked onto adjacent pavements. Sediment that is tracked will be removed and placed within the site or permanently disposed of offsite. A concrete washout will be used on site during the concrete placement. All hardened concrete will be disposed of offsite. These BMP's have not been located on the site map due to the fact that the site is very small and these BMP's will need to be placed by the contractor in locations that are most beneficial and will minimize disruption of adjacent traffic.

Permanent erosion control consists of covering the soils with a building, concrete walks, concrete drives and sod. No soil will be left exposed to erosion after the construction is complete. Refer to the landscape plan for areas of and instructions for placement of sod and soil amendments required prior to placement of sod.

Refer to Appendix D for the timing of the construction phases and the sequential installation of all BMP phasing for this site.

Refer to the Appendix E for the Erosion Control Surety calculations.

5.2 SWMP contact information

Permit holder:

Name: _____

Address: _____

Phone Number: _____

Email Address: _____

Appointed agent:

Name: _____

Address: _____

Phone Number: _____

Email Address: _____

5.3 Identification and location of all potential pollution sources

Potential Pollutant Source Activity	Potential Pollutant Generated	Applicable to this project
Disturbed Areas	Sediment	X
Soil stockpiles	Sediment	X
Travel to adjacent public streets	Tracked sediment	X
Contaminated soils	Sediment, chemicals	
Loading and unloading chemicals	Chemicals	
Unloading of building materials	Trash, debris	X
Outdoor storage of chemicals	Chemicals	
On site equipment maintenance	Oil, grease	
On site equipment fueling	Diesel, gasoline	X
Dust generating activities	Particulates, sediment	X
Use of fertilizer, pesticides, herbicides	Fertilizer, pesticides	
Use of detergents, solvents, oils	Detergents, solvents, oil	X
Waste dumpsters, waste piles	Chemicals, trash, debris	X
Concrete washout	Concrete, sediment, wash water	X
On site equipment washing	Detergents, oil	
On site asphalt batch plant	Asphaltic cement, sediment	
On site concrete batch plant	Cement, sediment	
Portable toilets	Domestic sewage	X

5.4 Best Management Practices (BMP's) for Stormwater Pollution Prevention

Structural Practices for Erosion and Sediment Control

Structural practices for the site will consist mainly of silt fence and rock sock filters and are described in detail in the following paragraphs. These BMP's are expected to change as the construction progresses and it is the responsibility of the contractor to ensure appropriate BMP's are in place and/or removed at the appropriate time in the construction sequence. All temporary and permanent erosion and sediment control practices must be maintained and repaired as needed to assure continued performance of their intended function.

Silt fence and rock sock filters shall be in place prior to commencement of construction activities. During clearing and grubbing necessary for silt fence installation, all cleared material shall be placed on the uphill side so that if erosion occurs from the cleared material, the sediment will be trapped and not transported downstream. Rock socks shall be implemented in the existing curb line as shown on the Drainage & Erosion Control Plan.

All BMP's shall be installed per the details shown on the construction plan set.

Temporary & Permanent Structural BMP's:

Structural BMP	Approximate location on site	Applicable to this Project
Silt Fence	Site perimeter, refer to site map	X
Straw bale dams		
Rock Socks	At existing sidewalk culverts, in existing gutters, refer to site map	X
Earthen diversion dams		
Vegetated swales		
Sediment trap/pond	East boundary of site, in proposed det pond	X
Pipe slope drains		
Geogrid		
Inlet/outlet protection	In the detention Pond	X
Culverts		
Riprap		
Erosion control mats		
Inlet protection		
Vehicle Tracking Control Pad	At site entrance, refer to site map	X
Concrete Washout	To be located by Contractor, near site entry	X

Non-Structural Practices for Erosion and Sediment Control:

Soils exposed during the earthwork phase and landscape prep phase shall be kept in a roughened condition by ripping or disking along land contours until mulch, vegetation, or other permanent erosion control is installed. No large amount of soils (in excess of 15 yards) will be allowed to be stock piled on site. Overburden from the utility pipe trenching will be piled adjacent to trenches upstream of sediment controls and will be replaced in the trenches within 72 hours.

Excess excavated materials from the demolition and grading phases of the project that cannot be reused on site will be exported as it is excavated. This includes any asphalt pavement from the existing site that is to be removed.

A vehicle tracking pad will be installed at a location most beneficial to the site construction as determined by the contractor. Vehicles will not be permitted in the excavated area if soil is muddy. Gravel sub base will be placed and compacted in the areas indicated for pavement following excavation. In the current pre construction state the site enables tracking of silt onto the adjacent streets during wet conditions. During construction activities the street will be monitored for foreign debris tracked out of the site and mechanical sweeping and clean up will be performed as needed.

No area shall remain exposed by land disturbing activity for more than thirty (30) days before required temporary or permanent erosion control (e.g. seed/mulch, landscaping, etc.) is installed.

Temporary & Permanent non-structural BMP's:

Non-Structural BMP	Approximate location on site	Applicable to this Project
Surface roughening	Entire site	X
Soil stockpile height limit (less than 10')		
Perimeter vegetative buffer	West and north boundaries of site	X
Minimization of site disturbance		
Mulch		
Seed & mulch stockpiles after 30 days		
Stockpile toe protection (silt fence, wattles or ditch)		
Preservation & protection of existing vegetation & trees	West and north boundaries of site	X
Good site housekeeping (routine cleanup of trash & constr debris)	Entire Site	X
Sweeping & scraping of hardscape areas	On and off site pavements	X
Heavy equip staged on site, properly maintained & inspected daily (no onsite maintenance)	Staging area	X

5.5 BMP Implementation

1) Phased BMP Implementation

BMP's are expected to change as the construction progresses and it is the responsibility of the contractor to ensure appropriate BMP's are in place and/or removed at the appropriate time in the construction sequence. A construction sequence schedule has been included on the Drainage & Erosion Control Plan and included in the construction plans for this site.

All BMP's shall be inspected and repaired or replaced as required to satisfy the conditions of the Stormwater Discharge Permit. All BMP's must be maintained and repaired as needed to assure continued performance of their intended function. Refer to Appendix D for the BMP schedule and estimated costs.

2) Materials Handling and Spill Prevention:

Materials Handling & Spill Prevention BMP	Approximate location on site	Applicable to this Project
Portable toilets, anchored & located away from drainages	Contractor to determine	X
Fuel storage located in bulk tanks with secondary containment & spill kit		
Mobile fueling performed at least 200 feet away from drainages & fully attended	Contractor to determine	X
Fertilizers, form oil, solvents, cleaners, detergent stored in 55 gal or smaller containers, kept in storage units	Contractor to determine	X
Dumpsters containing used chemicals containers & liquid wastes kept covered	Contractor to determine	X
Equipment cleaning (on site) uses no detergents & flows to onsite retention basin		
In case of a release of fuel or other chemicals, absorbent booms or earthen berms will be immediately constructed to contain the spill & prevent runoff to adjacent surface waters	Location of spill	X
MSDS sheets for onsite chemicals will be kept at the construction trailer to facilitate spill response & cleanup	Contractor to determine	X

3) Dedicated Asphalt or Concrete Batch Plant:

Not proposed with this development

4) Vehicle Tracking Pad:

Vehicle tracking control pad shall be installed wherever construction vehicle access routes intersect paved public roads. Vehicle tracking control pads shall be installed to minimize the transport of sediment (mud) by runoff or vehicles tracking onto the paved surface. Any mud tracked to public roads shall be removed on a daily basis and after any significant storm that causes sediment to be transported. It is unlawful to track sediment/mud onto public streets and may be enforced by the City of Fort Collins, by the State of Colorado or by the EPA.

5) Waste Management and Disposal:

Portable toilets will be anchored & periodically maintained by waste management company. Dumpsters on site will be covered & periodically emptied by waste management company. Concrete waste will be allowed to harden and then will be removed from site.

No washing activities will occur on site.

Location of the concrete washout is shown on the site map. The washout will be sufficiently deep to accommodate all anticipated concrete truck wash water. Waste concrete will be allowed to harden and be removed from site periodically as the washout reaches 50% of its capacity. Truck wash water will not be allowed to reach the curb & gutter or any other water course.

6) Groundwater and Stormwater Dewatering:

No groundwater was encountered during soils exploration therefore ground water is not anticipated to be an issue. If groundwater is encountered a groundwater discharge permit shall be obtained and a detailed report shall be completed describing the location and the route of where pumped groundwater will be conveyed and the measures taken to prevent the transport of any pollutants to downstream waters.

7) Inspection & Maintenance:

It is required that routine site inspections are performed to effectively address maintenance and repair of Best Management Practices (BMP's). The site inspections are to performed by the contractor or an inspector designated by the administrator at a minimum of once every fourteen (14) calendar days on active construction sites and after any significant storm event (an event causing runoff). As part of the site inspections the inspector is required to keep documentation of

all inspections and BMP maintenance, including an updated Site Map indicating new BMP's or the removal of BMP's since the previous inspection.

Any maintenance, repair, or necessary installation of BMP's that are noted during the inspection must be completed within seven (7) calendar days from the date of the inspection

6. CONCLUSIONS

6.1 Compliance with Standards

All computations that have been completed within this report are in compliance with the “City of Fort Collins Erosion Control Reference Manual for Construction Sites”, the “City of Fort Collins Storm Drainage Design Criteria Manual”, and the “Urban Storm Drainage Criteria Manual” except where variances are requested as noted in Section 4.2 of this report.

6.2 Drainage Concept

The proposed drainage concepts presented in this report and on the construction plans adequately provide for the collection and conveyance of on-site runoff to the detention area. Conveyance elements exist to adequately convey detained runoff downstream.

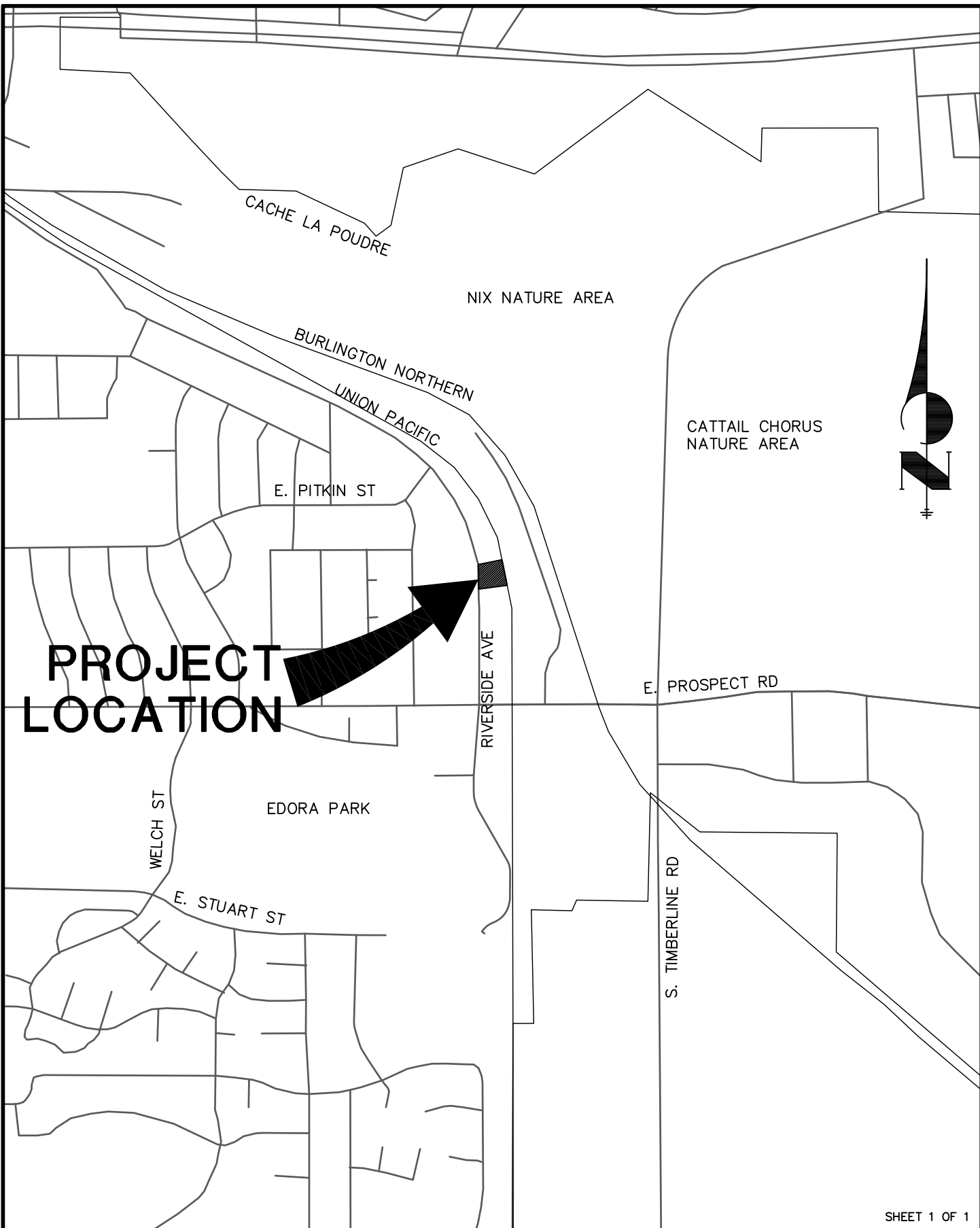
If, at the time of construction, groundwater is encountered, a Colorado Department of Health Construction Dewatering Permit would be required.

7. REFERENCES

1. City of Fort Collins, “Storm Drainage Criteria Manual”, (SDCM), dated March, 1986.
2. Urban Drainage and Flood Control District, “Urban Storm Drainage Criteria Manual”, Volumes 1 and 2, dated March, 1969, and Volume 3 dated September, 1992.

APPENDIX A

VICINITY MAP



**PROJECT
LOCATION**

SHEET 1 OF 1

DATE:	10/10/14
SCALE:	1"=1000'
DESIGNED BY:	PPK
JOB NO.:	264-03

**1640 RIVERSIDE DRIVE
(RIVERSIDE STORAGE)**

VICINITY MAP



700 Automation Drive, Unit I
Windsor, Colorado 80550
Phone: 970-686-6939
Fax: 970-686-1188

APPENDIX B

HYDROLOGIC COMPUTATIONS

RUNOFF COEFFICIENTS & % IMPERVIOUS

LOCATION: First Replat of Prospect Riverside Subdivision
 PROJECT NO: 264-03
 COMPUTATIONS BY: ppk
 DATE: 10/16/2014

Recommended Runoff Coefficients from Table 3-3 of City of Fort Collins Design Criteria
 Recommended % Impervious from Urban Storm Drainage Criteria Manual

	% Impervious	Runoff coefficient C
Streets, parking lots (asphalt):	100%	0.95
Sidewalks:	96%	0.95
Gravel:	40%	0.50
Roofs:	90%	0.95
Lawns (flat <2%, heavy soil):	0%	0.20

SUBBASIN DESIGNATION	TOTAL AREA (ac.)	TOTAL AREA (sq.ft)	ROOF AREA (sq.ft)	PAVED AREA (sq.ft)	SIDEWALK AREA (sq.ft)	GRAVEL AREA (sq.ft)	LANDSCAPE AREA (sq.ft)	% Impervious	RUNOFF COEFF. (C)
Existing	2.18	95,094	0	17,700	0	19,530	57,864	30%	0.46
Proposed	2.18	95,094	31,743	38,365	1,763	0	23,223	72%	0.77

Equations

- Calculated C coefficients & % Impervious are area weighted

$$C = \sum (C_i A_i) / A_t$$

C_i = runoff coefficient for specific area, A_i

A_i = areas of surface with runoff coefficient of C_i

n = number of different surfaces to consider

A_t = total area over which C is applicable; the sum of all A_i 's

STANDARD FORM SF-2
TIME OF CONCENTRATION - 2 YEAR

LOCATION: First Replat of Prospect Riverside Subdivision
 PROJECT NO: 264-03
 COMPUTATIONS BY: ppk
 DATE: 10/16/2014

2-yr storm Cf = 1.00

SUB-BASIN DATA			INITIAL /OVERLAND TIME (ti)				TRAVEL TIME / GUTTER OR CHANNEL FLOW (tt)						tc CHECK (URBANIZED BASIN)		FINAL tc	REMARKS
DESIGN POINT	SUBBASIN(s) (1)	Area (ac) (2)	C (3)	Length (ft) (4)	Slope (%) (5)	ti (min) (6)	Length (ft) (7)	Slope (%) (8)	n Manning rough. (9)	Vel. (ft/s) (10)	tt (min) (11)	tc = ti + tt (11)	Total L (ft) (12)	tc=(L/180)+10 (min) (13)	(min) (14)	
1	Existing	2.18	0.46	225	2.8	12.2	225	1.6	0.030	1.4	2.77	15.0	450	12.5	12.5	
1	Proposed	2.18	0.77	66	1.0	4.9	406	0.6	0.016	1.6	4.35	9.2	472	12.6	9.2	

EQUATIONS:

tc = ti + tt

ti = $[1.87 (1.1 - CC_f) L^{0.5}] / S^{1/3}$

tt = L/Vel. Velocity from Manning's Equation with R=0.1 (corresponds to Figure 3-3 of City of Fort Collins Design Manual)

final tc = minimum of ti + tt and urbanized basin check
 min. tc = 5 minutes

STANDARD FORM SF-2
TIME OF CONCENTRATION - 100 YR

LOCATION: First Replat of Prospect Riverside Subdivision
 PROJECT NO: 264-03
 COMPUTATIONS BY: ppk
 DATE: 10/16/2014

100-yr storm Cf = 1.25

SUB-BASIN DATA			INITIAL /OVERLAND TIME (ti)					TRAVEL TIME / GUTTER OR CHANNEL FLOW (tt)						tc CHECK (URBANIZED BASIN)		FINAL tc	REMARKS
DESIGN POINT	SUBBASIN(s) (1)	Area (ac) (2)	C (3)	C*Cf	Length (ft) (4)	Slope (%) (5)	ti (min) (6)	Length (ft) (7)	Slope (%) (8)	n Manning rough.	Vel. (ft/s) (9)	tt (min) (10)	tc = ti + tt (11)	Total L (ft) (12)	tc=(l/180)+10 (min) (13)	(min) (14)	
1	Existing	2.18	0.46	0.58	225	2.8	10.0	225	1.6	0.030	1.4	2.77	12.8	450	12.5	12.5	
1	Proposed	2.18	0.77	0.96	66	1.0	2.1	406	0.6	0.016	1.6	4.35	6.4	472	12.6	6.4	

EQUATIONS:

tc = ti + tt

ti = [1.87 (1.1 - CC_r) L^{0.5}] / S^{1/3}

tt = L/Vel. Velocity from Manning's Equation with R=0.1 (corresponds to Figure 3-3 of City of Fort Collins Design Manual)

final tc = minimum of ti + tt and urbanized basin check
 min. tc = 5 minutes

RATIONAL METHOD PEAK RUNOFF (2-YEAR)

LOCATION: First Replat of Prospect Riverside Subdivision
 PROJECT NO: 264-03
 COMPUTATIONS BY: ppk
 DATE: #####

2-yr storm, Cf = 1.00

Design Point	Tributary Sub-basin	DIRECT RUNOFF					CARRY OVER		TOTAL	REMARKS
		A (ac)	C*Cf	tc (min)	i (new) (in/hr)	Q (2) (cfs)	from Design Point	Q (2) (cfs)	Q(2)tot (cfs)	
1	Existing	2.18	0.46	12.5	2.02	2.0			2.0	Allowable pond release
1	Proposed	2.18	0.77	9.2	2.28	3.8			3.8	

$$Q = C_f C i A$$

- Q = peak discharge (cfs)
- C = runoff coefficient
- C_f = frequency adjustment factor
- i = rainfall intensity (in/hr) from IDF curve
- A = drainage area (acres)

**RATIONAL METHOD PEAK RUNOFF
 (100-YEAR)**

LOCATION: First Replat of Prospect Riverside Subdivision
 PROJECT NO: 264-03
 COMPUTATIONS BY: ppk
 DATE: #####

100-yr storm, Cf = 1.25

Des. Point	Area Design.	DIRECT RUNOFF					CARRY OVER		TOTAL	REMARKS
		A (ac)	C*Cf	tc (min)	i (new) (in/hr)	Q (100) (cfs)	from Design Point	Q (100) (cfs)	Q(100)tot (cfs)	
1	Existing	2.18	0.58	12.5	7.03	8.9			8.9	
1	Proposed	2.18	0.96	6.4	9.04	18.9			18.9	

$Q = CiA$

Q = peak discharge (cfs)
 C = runoff coefficient
 I = rainfall intensity (in/hr) from IDF curve
 A = drainage area (acres)

APPENDIX C

DETENTION POND SIZING CALCULATIONS

Detention Pond Outlet Sizing
(100 yr event)

LOCATION: First Replat of Prospect Riverside Subdivision
 PROJECT NO: 264-02
 COMPUTATIONS BY: PPK
 SUBMITTED BY: North Star Design, Inc.
 DATE: #####

Submerged Orifice Outlet:

release rate is described by the orifice equation,

$$Q_o = C_o A_o \sqrt{2g(h-E_o)}$$

where Q_o = orifice outflow (cfs)
 C_o = orifice discharge coefficient
 g = gravitational acceleration = 32.2 ft/s
 A_o = effective area of the orifice (ft²)
 E_o = greater of geometric center elevation of the orifice or d/s HGL (ft)
 h = water surface elevation (ft)

$Q_o = 2.0$ cfs
 outlet pipe dia = $D = 12.0$ in
 Invert elev. = 4934.30 ft
 $E_o = 4934.63$ ft
 $h = 4936.10$ ft - 100 yr WSEL
 $C_o = 0.62$

solve for effective area of orifice using the orifice equation

$A_o = 0.331$ ft²
 = 47.7 in²
 orifice dia. = $d = 7.79$ in

Check orifice discharge coefficient using Figure 5-21 (*Hydraulic Engineering*)

$d / D = 0.65$
 kinematic viscosity, $\nu = 1.22E-05$ ft²/s
 Reynolds no. = $Re_d = 4Q/(p\nu) = 3.21E+05$
 $C_o = (K \text{ in figure}) = 0.62$ check

Use $d = 7.80$ in
 $A_o = 0.332$ ft² = 47.78 in²
 $Q_{max} = 2.0$ cfs

DETENTION VOLUME BY THE MODIFIED FAA METHOD

Project: Riverside storage

Basin ID: 1

(For catchments less than 160 acres only. For larger catchments, use hydrograph routing method)
 (NOTE: for catchments larger than 90 acres, CUHP hydrograph and routing are recommended)

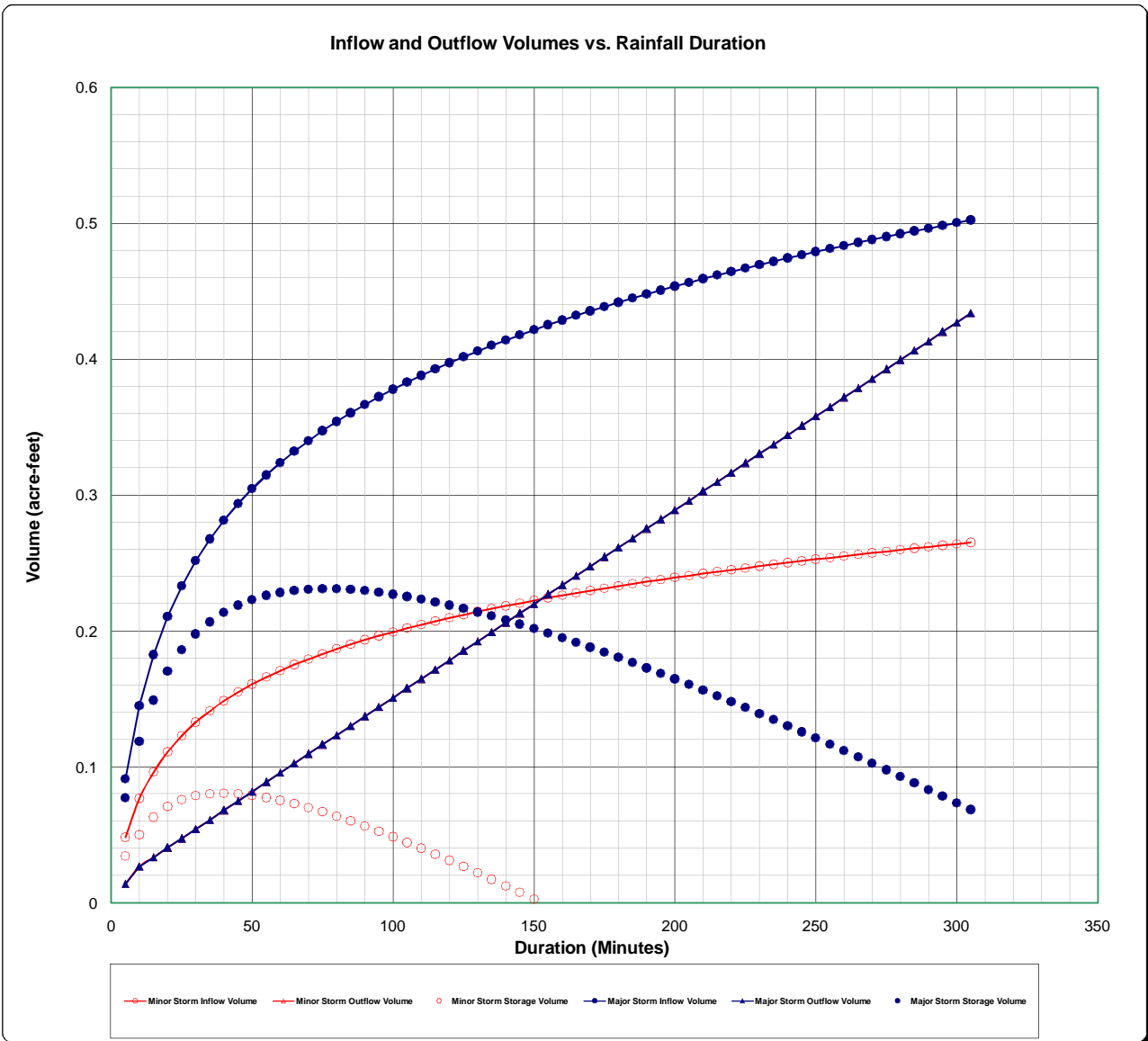
Determination of MINOR Detention Volume Using Modified FAA Method							Determination of MAJOR Detention Volume Using Modified FAA Method						
Design Information (Input): Catchment Drainage Imperviousness $I_p = 72.00$ percent Catchment Drainage Area $A = 2.180$ acres Predevelopment NRCS Soil Group Type = C A, B, C, or D Return Period for Detention Control $T = 10$ years (2, 5, 10, 25, 50, or 100) Time of Concentration of Watershed $T_c = 9$ minutes Allowable Unit Release Rate $q = 0.92$ cfs/acre One-hour Precipitation $P_1 = 1.61$ inches Design Rainfall IDF Formula $i = C_1 \cdot P_1 / (C_2 + T_c)^{C_3}$ Coefficient One $C_1 = 28.50$ Coefficient Two $C_2 = 10$ Coefficient Three $C_3 = 0.789$							Design Information (Input): Catchment Drainage Imperviousness $I_p = 72.00$ percent Catchment Drainage Area $A = 2.180$ acres Predevelopment NRCS Soil Group Type = C A, B, C, or D Return Period for Detention Control $T = 100$ years (2, 5, 10, 25, 50, or 100) Time of Concentration of Watershed $T_c = 9$ minutes Allowable Unit Release Rate $q = 0.92$ cfs/acre One-hour Precipitation $P_1 = 2.61$ inches Design Rainfall IDF Formula $i = C_1 \cdot P_1 / (C_2 + T_c)^{C_3}$ Coefficient One $C_1 = 28.50$ Coefficient Two $C_2 = 10$ Coefficient Three $C_3 = 0.789$						
Determination of Average Outflow from the Basin (Calculated): Runoff Coefficient $C = 0.59$ Inflow Peak Runoff $Q_{p-in} = 5.73$ cfs Allowable Peak Outflow Rate $Q_{p-out} = 2.01$ cfs Mod. FAA Minor Storage Volume = 3.507 cubic feet Mod. FAA Minor Storage Volume = 0.081 acre-ft							Determination of Average Outflow from the Basin (Calculated): Runoff Coefficient $C = 0.69$ Inflow Peak Runoff $Q_{p-in} = 10.87$ cfs Allowable Peak Outflow Rate $Q_{p-out} = 2.01$ cfs Mod. FAA Major Storage Volume = 10.059 cubic feet Mod. FAA Major Storage Volume = 0.231 acre-ft						
5 <- Enter Rainfall Duration Incremental Increase Value Here (e.g. 5 for 5-Minutes)													
Rainfall Duration (input) minutes	Rainfall Intensity (output) inches / hr	Inflow Volume (output) acre-feet	Adjustment Factor "m" (output)	Average Outflow (output) cfs	Outflow Volume (output) acre-feet	Storage Volume (output) acre-feet	Rainfall Duration (input) minutes	Rainfall Intensity (output) inches / hr	Inflow Volume (output) acre-feet	Adjustment Factor "m" (output)	Average Outflow (output) cfs	Outflow Volume (output) acre-feet	Storage Volume (output) acre-feet
5	5.42	0.048	1.00	2.01	0.014	0.034	5	8.78	0.091	1.00	2.01	0.014	0.077
10	4.32	0.076	0.96	1.93	0.027	0.050	10	7.00	0.145	0.96	1.93	0.027	0.118
15	3.62	0.096	0.81	1.62	0.033	0.063	15	5.87	0.182	0.81	1.62	0.033	0.149
20	3.13	0.111	0.73	1.46	0.040	0.071	20	5.08	0.211	0.73	1.46	0.040	0.170
25	2.78	0.123	0.68	1.37	0.047	0.076	25	4.50	0.233	0.68	1.37	0.047	0.186
30	2.50	0.133	0.65	1.31	0.054	0.079	30	4.05	0.252	0.65	1.31	0.054	0.198
35	2.28	0.141	0.63	1.27	0.061	0.080	35	3.69	0.268	0.63	1.27	0.061	0.207
40	2.09	0.148	0.62	1.23	0.068	0.081	40	3.40	0.281	0.62	1.23	0.068	0.214
45	1.94	0.155	0.60	1.21	0.075	0.080	45	3.15	0.294	0.60	1.21	0.075	0.219
50	1.81	0.161	0.59	1.19	0.082	0.079	50	2.94	0.305	0.59	1.19	0.082	0.223
55	1.70	0.166	0.58	1.17	0.089	0.077	55	2.76	0.315	0.58	1.17	0.089	0.226
60	1.61	0.171	0.58	1.16	0.096	0.075	60	2.60	0.324	0.58	1.16	0.096	0.228
65	1.52	0.175	0.57	1.14	0.102	0.073	65	2.47	0.332	0.57	1.14	0.102	0.230
70	1.45	0.179	0.57	1.13	0.109	0.070	70	2.34	0.340	0.57	1.13	0.109	0.231
75	1.38	0.183	0.56	1.13	0.116	0.067	75	2.23	0.347	0.56	1.13	0.116	0.231
80	1.32	0.187	0.56	1.12	0.123	0.064	80	2.14	0.354	0.56	1.12	0.123	0.231
85	1.26	0.190	0.55	1.11	0.130	0.060	85	2.05	0.360	0.55	1.11	0.130	0.230
90	1.21	0.193	0.55	1.11	0.137	0.056	90	1.97	0.367	0.55	1.11	0.137	0.229
95	1.17	0.196	0.55	1.10	0.144	0.052	95	1.89	0.372	0.55	1.10	0.144	0.228
100	1.12	0.199	0.55	1.10	0.151	0.048	100	1.82	0.378	0.55	1.10	0.151	0.227
105	1.09	0.202	0.54	1.09	0.158	0.044	105	1.76	0.383	0.54	1.09	0.158	0.225
110	1.05	0.205	0.54	1.09	0.165	0.040	110	1.70	0.388	0.54	1.09	0.165	0.223
115	1.02	0.207	0.54	1.08	0.172	0.036	115	1.65	0.393	0.54	1.08	0.172	0.221
120	0.99	0.210	0.54	1.08	0.178	0.031	120	1.60	0.397	0.54	1.08	0.178	0.219
125	0.96	0.212	0.54	1.08	0.185	0.027	125	1.55	0.402	0.54	1.08	0.185	0.216
130	0.93	0.214	0.54	1.07	0.192	0.022	130	1.51	0.406	0.54	1.07	0.192	0.214
135	0.90	0.216	0.53	1.07	0.199	0.017	135	1.47	0.410	0.53	1.07	0.199	0.211
140	0.88	0.218	0.53	1.07	0.206	0.012	140	1.43	0.414	0.53	1.07	0.206	0.208
145	0.86	0.220	0.53	1.07	0.213	0.007	145	1.39	0.418	0.53	1.07	0.213	0.205
150	0.84	0.222	0.53	1.06	0.220	0.002	150	1.36	0.422	0.53	1.06	0.220	0.202
155	0.82	0.224	0.53	1.06	0.227	-0.003	155	1.32	0.425	0.53	1.06	0.227	0.198
160	0.80	0.226	0.53	1.06	0.234	-0.008	160	1.29	0.429	0.53	1.06	0.234	0.195
165	0.78	0.228	0.53	1.06	0.241	-0.013	165	1.26	0.432	0.53	1.06	0.241	0.191
170	0.76	0.230	0.53	1.06	0.248	-0.018	170	1.24	0.435	0.53	1.06	0.248	0.188
175	0.75	0.231	0.53	1.06	0.254	-0.023	175	1.21	0.439	0.53	1.06	0.254	0.184
180	0.73	0.233	0.53	1.05	0.261	-0.028	180	1.18	0.442	0.53	1.05	0.261	0.180
185	0.72	0.235	0.52	1.05	0.268	-0.034	185	1.16	0.445	0.52	1.05	0.268	0.177
190	0.70	0.236	0.52	1.05	0.275	-0.039	190	1.14	0.448	0.52	1.05	0.275	0.173
195	0.69	0.238	0.52	1.05	0.282	-0.044	195	1.12	0.451	0.52	1.05	0.282	0.169
200	0.68	0.239	0.52	1.05	0.289	-0.050	200	1.09	0.454	0.52	1.05	0.289	0.165
205	0.66	0.241	0.52	1.05	0.296	-0.055	205	1.07	0.456	0.52	1.05	0.296	0.160
210	0.65	0.242	0.52	1.05	0.303	-0.061	210	1.06	0.459	0.52	1.05	0.303	0.156
215	0.64	0.244	0.52	1.05	0.310	-0.066	215	1.04	0.462	0.52	1.05	0.310	0.152
220	0.63	0.245	0.52	1.04	0.317	-0.072	220	1.02	0.464	0.52	1.04	0.317	0.148
225	0.62	0.246	0.52	1.04	0.323	-0.077	225	1.00	0.467	0.52	1.04	0.323	0.143
230	0.61	0.248	0.52	1.04	0.330	-0.083	230	0.99	0.469	0.52	1.04	0.330	0.139
235	0.60	0.249	0.52	1.04	0.337	-0.088	235	0.97	0.472	0.52	1.04	0.337	0.135
240	0.59	0.250	0.52	1.04	0.344	-0.094	240	0.95	0.474	0.52	1.04	0.344	0.130
245	0.58	0.251	0.52	1.04	0.351	-0.100	245	0.94	0.477	0.52	1.04	0.351	0.126
250	0.57	0.253	0.52	1.04	0.358	-0.105	250	0.92	0.479	0.52	1.04	0.358	0.121
255	0.56	0.254	0.52	1.04	0.365	-0.111	255	0.91	0.481	0.52	1.04	0.365	0.116
260	0.55	0.255	0.52	1.04	0.372	-0.117	260	0.90	0.484	0.52	1.04	0.372	0.112
265	0.55	0.256	0.52	1.04	0.379	-0.122	265	0.88	0.486	0.52	1.04	0.379	0.107
270	0.54	0.257	0.52	1.04	0.386	-0.128	270	0.87	0.488	0.52	1.04	0.386	0.102
275	0.53	0.259	0.52	1.04	0.393	-0.134	275	0.86	0.490	0.52	1.04	0.393	0.098
280	0.52	0.260	0.52	1.04	0.399	-0.140	280	0.85	0.492	0.52	1.04	0.399	0.093
285	0.52	0.261	0.52	1.04	0.406	-0.146	285	0.84	0.494	0.52	1.04	0.406	0.088
290	0.51	0.262	0.52	1.03	0.413	-0.151	290	0.83	0.496	0.52	1.03	0.413	0.083
295	0.50	0.263	0.52	1.03	0.420	-0.157	295	0.82	0.498	0.52	1.03	0.420	0.078
300	0.50	0.264	0.52	1.03	0.427	-0.163	300	0.81	0.500	0.52	1.03	0.427	0.073
305	0.49	0.265	0.52	1.03	0.434	-0.169	305	0.79	0.502	0.52	1.03	0.434	0.068
Mod. FAA Minor Storage Volume (cubic ft.) = 3,507 Mod. FAA Minor Storage Volume (acre-ft.) = 0.0805							Mod. FAA Major Storage Volume (cubic ft.) = 10,059 Mod. FAA Major Storage Volume (acre-ft.) = 0.2309						

UDFCD DETENTION BASIN VOLUME ESTIMATING WORKBOOK Version 2.34, Released November 2013

DETENTION VOLUME BY THE MODIFIED FAA METHOD

Project: Riverside storage

Basin ID: 1



**STAGE - STORAGE TABLE
(100-YEAR)**

LOCATION: First Replat of Prospect Riverside Subdivision
 PROJECT NO: 264-02
 COMPUTATIONS BY: PPK
 SUBMITTED BY: North Star Design, Inc.
 DATE: 8/1/2008

100 yr Detention Volume Required = 0.231

Water Quality Volume Required = 0.075

Total Volume Required= 0.306

Stage (ft)	Surface Area (ft ²)	Incremental Storage (ac-ft)	Total Storage (ac-ft)
4934.30	0		
4935.0	7,850	0.042	0.04
<i>WQCV</i> 4935.17	8,801	0.032	0.075
4936.0	13,442	0.242	0.284
<i>100 WSEL</i> 4936.10	15,105	0.033	0.316
4937.0	30,070	0.487	0.770

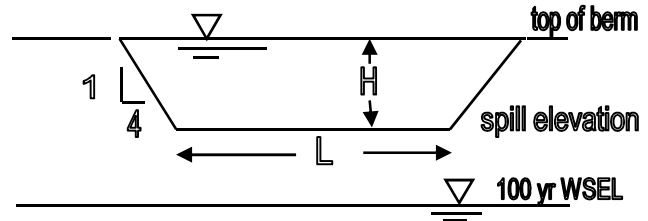
Emergency Overflow Spillway Sizing

LOCATION: First Replat of Prospect Riverside Subdivision
 PROJECT NO: 264-02
 COMPUTATIONS BY: PPK
 SUBMITTED BY: North Star Design, Inc.
 DATE: 5/24/2005

Equation for flow over a broad crested weir

$$Q = CLH^{3/2}$$

where C = weir coefficient = 2.8
 H = overflow height
 L = length of the weir



The pond has a spill elevation 0 ft above the maximum water surface elevation in the pond
 Spillways will be designed with 0.25 ft flow depth, thus H = 0.25 ft
 Size the spillway assuming that the pond outlet is completely clogged.

Q (100) =	18.9	cfs	
Spill elev =	4936.35	ft	100 yr WSEL = 4936.10 ft
Top of berm elev. =	4937.00		
Weir length required:			
L =	54	ft	
Use L =	55	ft	
v =	1.20	ft/s	

APPENDIX D

BMP SCHEDULE & COST ESTIMATE

Example Erosion and Sediment Control Escrow/Security Calculation for The City of Fort Collins

Project:

Riverside Storage

Disturbed Acres: 2.18

BMP Amount				
EROSION CONTROL BMPs	Units	Estimated Quantity	Unit Price	Total Price
Silt Fence	L.F.	1300	\$3.00	\$3,900.00
Rock Sock	each	15	\$85.00	\$1,275.00
Vehicle Tracking Control Pad	each	1	\$1,500.00	\$1,500.00
Concrete Washout	each	1	\$1,200.00	\$1,200.00
Rock Berm	each	1	\$65.00	\$65.00

(add all other BMPs for the site in this list)

Sub-Total: \$7,940.00
 1.5 x Sub-Total: \$11,910.00
Amount of security: \$11,910.00

Reseeding Amount			
		Total Acres x Price/acre:	\$2,616.00
Unit Price of Seeding per acre:	\$1,200.00	Sub-Total:	\$2,616.00
		1.5 x Sub-Total:	\$3,924.00
		Amount to Re-seed:	\$3,924.00

Minimum Escrow Amount	
	Minimum escrow amount: \$3,000.00

Final Escrow Amount	
	Erosion Control Escrow: \$11,910.00

“The amount of the security must be based on one and one-half times the estimate of the cost to install the approved measures, or one and one-half times the cost to re-vegetate the disturbed land to dry land grasses based upon unit cost determined by the City's Annual Revegetation and Stabilization Bid, whichever is greater. In no instance, will the amount of security be less than one thousand five hundred dollars (\$1,500) for residential development or three thousand dollars (\$3,000) for commercial development”